



Quasi-stationary WAVEWATCH III

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Atmospheric and Oceanic Science

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Covered in this lecture:

- Action balance equation and solution methods
- Quasi-stationary operation of WWIII
- Alternative QS approaches
- Field case: Hurricane Gustav



Action balance equation



$$\frac{\partial N}{\partial t} + \nabla_x \cdot \dot{\mathbf{x}} N + \frac{\partial}{\partial k} \dot{k} N + \frac{\partial}{\partial \theta} \dot{\theta} N = \frac{S}{\sigma}$$
$$\dot{\mathbf{x}} = \mathbf{c}_g + \mathbf{U} ,$$
$$\dot{\mathbf{k}} = -\frac{\partial \sigma}{\partial d} \frac{\partial d}{\partial s} - \mathbf{k} \cdot \frac{\partial \mathbf{U}}{\partial s} , \quad \dot{\mathbf{\theta}} = -\frac{1}{k} \left[\frac{\partial \sigma}{\partial d} \frac{\partial d}{\partial m} - \mathbf{k} \cdot \frac{\partial \mathbf{U}}{\partial m} \right]$$

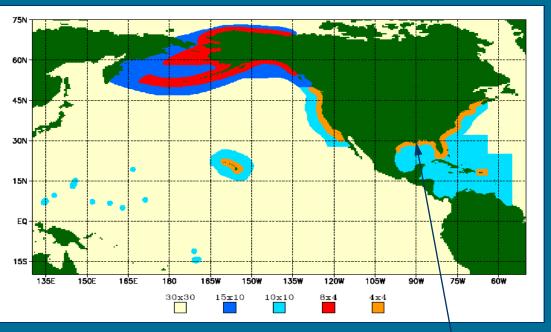
- Required physics for nearshore application already present
- Eulerian approach on rectangular, curvilinear or unstructured grids
- Explicit vs. Implicit implementations
- CFL constraints and nearshore application





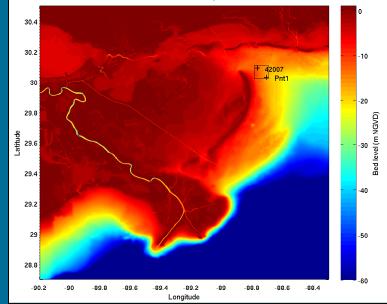
Current WWIII model grid mosaic

Desired nearshore application



Max. coastal resolution = 4 arc min (7.5 km)

bsndo: NX =761: NY =721, 250 m



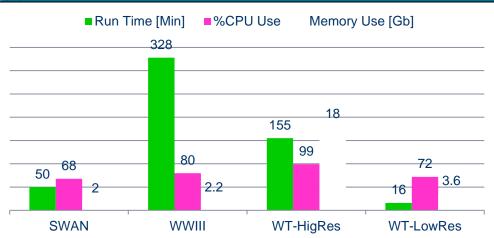
Nearshore resolution: < 100 m

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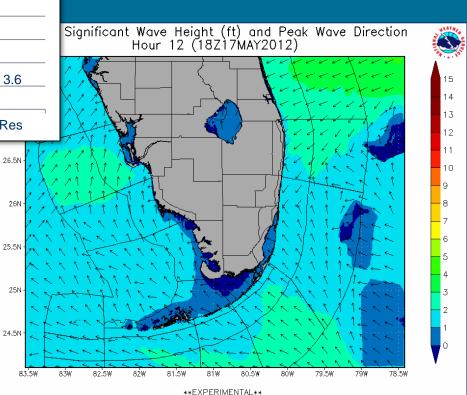
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Performance comparison: Explicit vs. Implicit





- WFO MFL Alpha testing site
- 1 arc-min grid
- 96 h forecast, dt 600 s





Quasi-stationary operation of WWIII

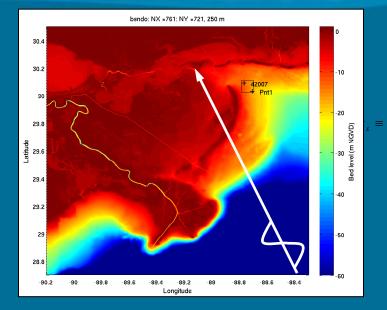


 $t_s \equiv$ Residence time $\Delta t_s \equiv$ Global input/output interval

Quasi-stationary conditions

where:

$$\gamma = \frac{\Delta t_s}{t_s} > 1$$



Time stepping can be accelerated: $t_i =$

$$t_i = t_{i-1} + \gamma \Delta t_n$$

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where

$$t_s = \alpha \frac{\text{Distance}}{\text{Group velocity}} = \alpha \frac{X}{c_{g,\tilde{T}m01}}$$

with α a constant = 1.2

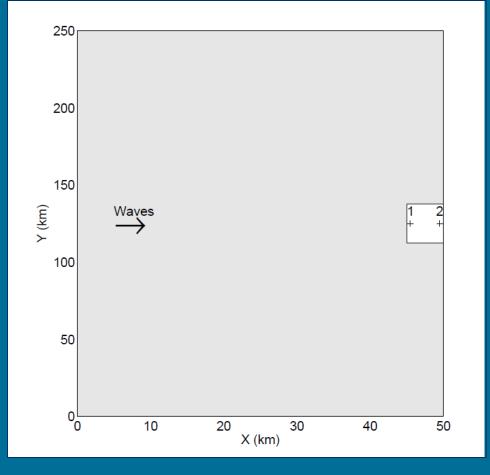
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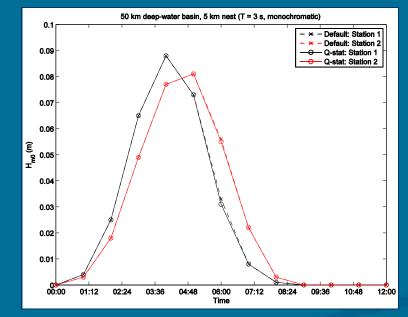
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Test case: Idealized wave propagation







 $f_p = 0.33$ Hz, Std dev. = 0.01 Hz Dir = 270 °N, monochromatic, long-crested

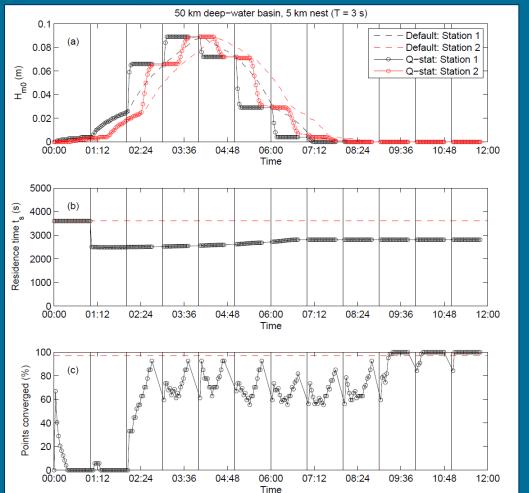
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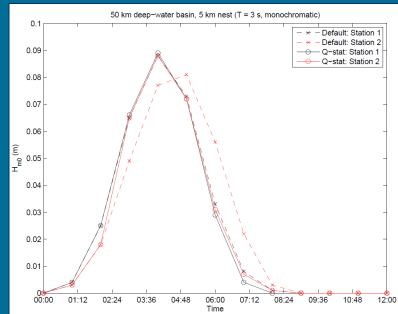
Approach 1: Discontinuous time stepping, discontinuous stationary BC





$$t_{i} = t_{0} + \left[i + \left(n_{m} - n_{i} \right) \left[\frac{i}{n_{i}} \right] \right] \Delta t_{n}$$

 $\psi_i = \psi_1$



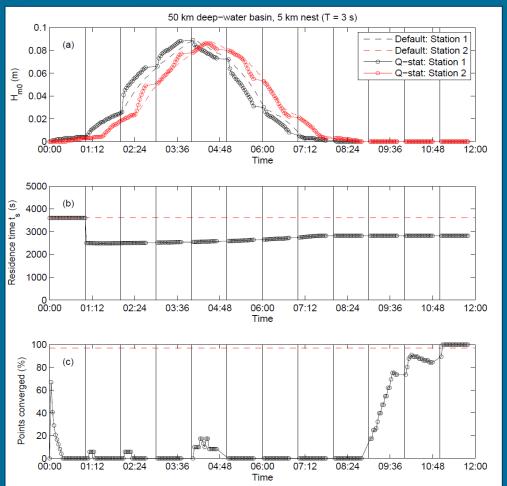
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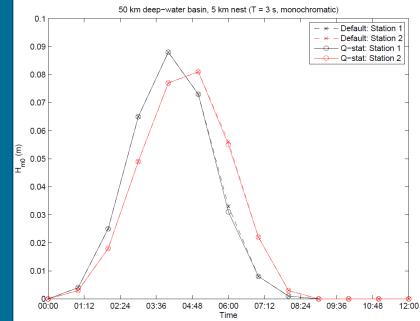
Approach 2: Discontinuous time stepping, discontinuous nonstationary, phase-shifted BC





$$t_{i} = t_{0} + \left[i + \left(n_{m} - n_{i} \right) \right] \frac{i}{n_{i}} \right] \Delta t_{n}$$

$$\psi_i = \psi \left(t_i + \left(\Delta t_s - t_s \right) \right) , \text{ for } \gamma > 1$$



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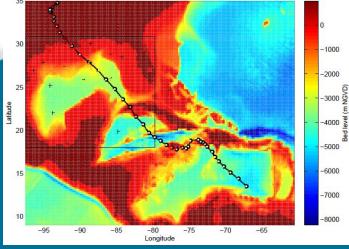
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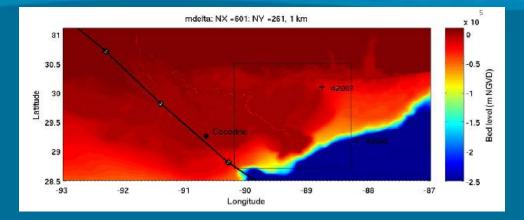
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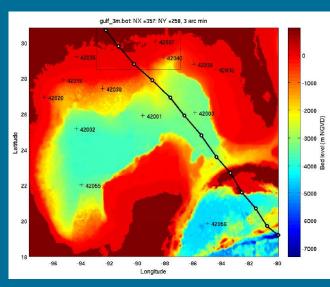
Field case: Hurricane Gustav (Aug-Sept 2008)

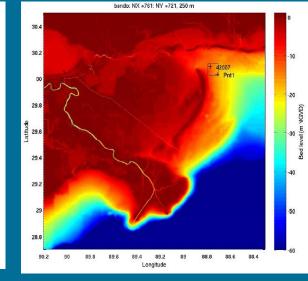


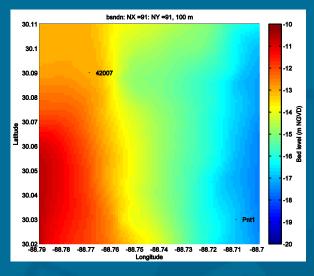












Data: Chen et al. (2010)

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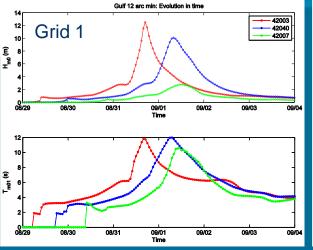
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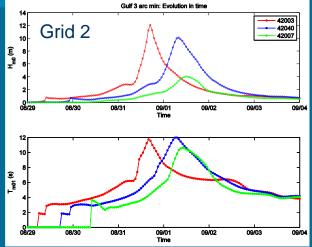
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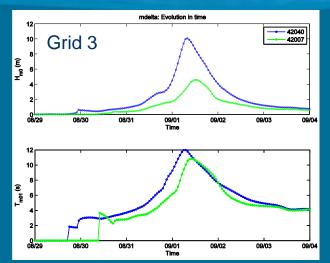


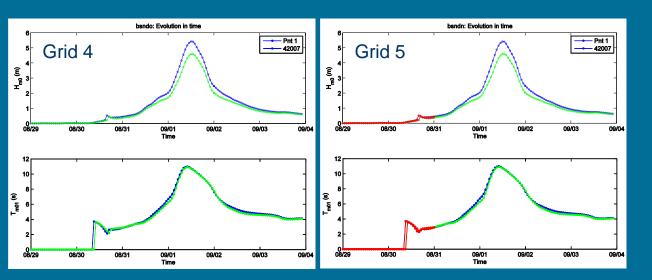
Results: H Gustav (Nonstationary WWIII)











Grid 5: ∆t_n = 5 s

Run time = 67 min (512 cores on IBM Power6 Cluster)

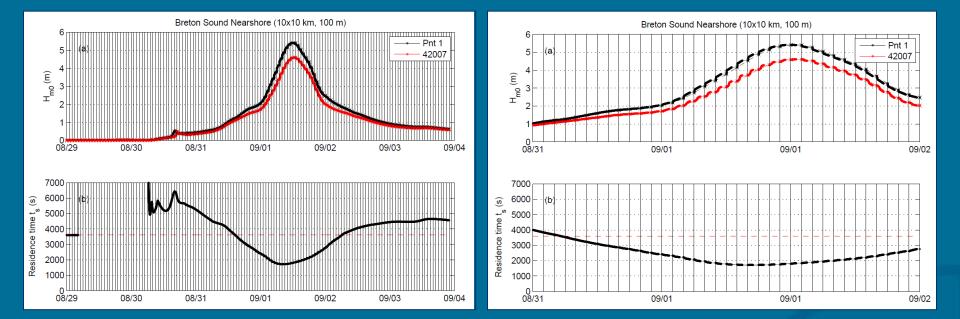
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Results: Hurricane Gustav, QS WWIII





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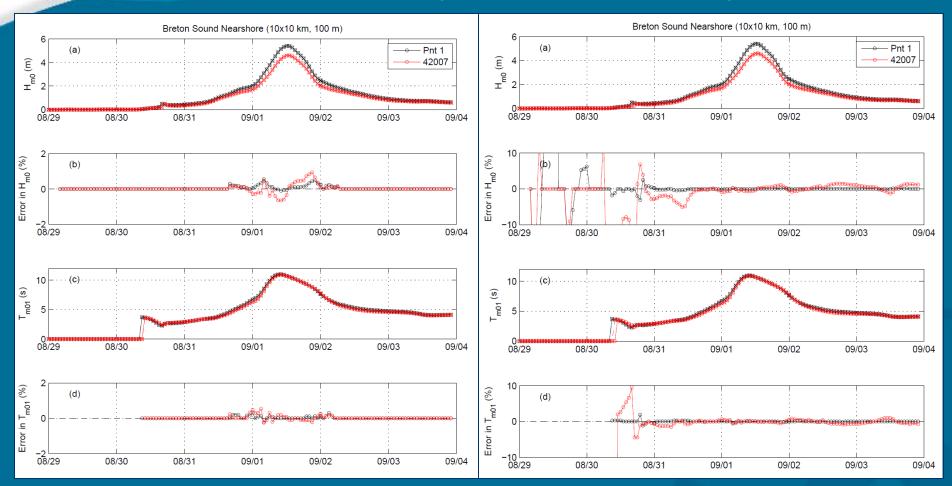


Results: Hurricane Gustav, QS WWIII



Wave-field dependent t_s

Constant $t_s = 1800 s$



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Conclusions



- If the residence time t_s in nearshore domains is shorter than the input/output interval, quasi-stationary conditions develop, and a saving in computational time of the explicit model is possible.
- Quasi-stationary approach is proposed with (i) discontinuous time stepping, and (ii) nonstationary, discontinuous, phase-shifted BCs.
- With variable t_s computed from wave field: Local computational time savings of up to 50% (depending on domain and wave condition), with errors below 1% and no spurious phase lag.
- With constant t_s : Greater constant savings in computational time (50% total), but with greater error (H_{m0} < 5%; T_{m01} < 2%).
- Run time is about 20 times longer than an equivalent nonstationary SWAN run (with ∆t = 10 min, no. iter = 3), but CFL condition is adhered to, and error can be controlled.
- Future: QS implementation for WWIII Multigrid.







End of lecture

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